

## **EFFECT OF DISPERSING LITHIUM GREASE BY ALUMINUM OXIDE NANOPARTICLES AND CARBON NANOTUBES**

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### **ABSTRACT**

The effect of dispersing lithium grease by aluminum oxide ( $\text{Al}_2\text{O}_3$ ) nanoparticles and carbon nanotubes (CNT) on the lubricating properties is discussed. Friction coefficient and wear displayed by the reciprocating sliding of bearing steel ball on aluminum (Al) sheet lubricated by lithium grease dispersed by  $\text{Al}_2\text{O}_3$  nanoparticles and CNT.

It was found that friction coefficient displayed by the grease dispersed by CNT displayed the highest values followed by  $\text{Al}_2\text{O}_3$ , while CNT/ $\text{Al}_2\text{O}_3$  showed the lowest values. Minimum values were observed at 0.4 – 0.6 wt. % of nanomaterial content. Minimum wear values were displayed by grease dispersed by CNT/ $\text{Al}_2\text{O}_3$  of 0.4 wt. % content. Further increase in  $\text{Al}_2\text{O}_3$  content significantly increased wear due to their abrasive action. It was observed that combination of CNT/ $\text{Al}_2\text{O}_3$  significantly reduced of friction and wear. That can be explained on the bases that agglomeration of CNT increased their layers and shear stress.  $\text{Al}_2\text{O}_3$  showed relatively lower increase in friction due to the ball bearing effect of the nanoparticles. The enhancing effect of CNT/ $\text{Al}_2\text{O}_3$  may be attributed to the easy rolling of  $\text{Al}_2\text{O}_3$  nanoparticles by the help of the low shear CNT.

### **KEYWORDS**

Aluminum oxide nanoparticles, carbon nanotubes, lithium grease.

### **INTRODUCTION**

Solid lubricants are extensively used to increase the efficiency of greases in different application. Polymeric particles dispersed in grease was proposed, [1, 2]. Their function is to adhere into the sliding surfaces, where the adhesion force depends on their deformed contact area that increases for soft polymers. Relatively harder polymers roll on the sliding surfaces decreasing friction and. Intensive care should be considered in selecting the solid lubricants suitable for dispersing greases. Rolling contact wear is familiar for rolling bearings, [3 - 5]. Increasing load carrying capacity of journal bearing running

under mixed lubricating condition is to apply extreme pressure (EP) additives. Polytetrafluoroethylene (PTFE) was dispersing grease.

Type of the lubricants mainly influences the lubrication of sliding surfaces, [6 - 9]. In metal forming, the relative movement between the tools and the work piece is accompanied by friction that controls the surface quality. Applying the proper lubricants can reduce the drawbacks of the friction. Friction was measured by sensors during metal forming process, [10 – 12]. It was found that engineering materials are sensitive to the contact pressure. The possibilities to evaluate friction were discussed, [13, 14]. Recently, it was found that friction coefficient displayed by the grease dispersed by multiwall carbon nanotubes (MWCNT) showed lower values than that dispersed by silica nanoparticles, [15]. Wear resistance provided by silica nanoparticles was superior to that observed for MWCNT.

The present work discusses the effect of dispersing lithium grease by  $\text{Al}_2\text{O}_3$  nanoparticles and CNT on friction coefficient and wear displayed by the sliding of bearing steel ball on aluminum sheet.

#### EXPERIMENTAL

The test rig used in the present experiments consists of bearing steel ball sliding on aluminum sheet in multiple passes under different load values, Figs. 1 and 2. Experiments were carried out to investigate the effect of the tested nanomaterials dispersing lithium grease on friction coefficient and wear. Weights of 2, 4, 6, 8, 10 and 12 N were vertically applied. Wear scar width was measured using optical microscope of  $\pm 0.01$  mm accuracy. The test was conducted manually under dry condition at room temperature. The stroke was 20 mm and repeated 10 times.

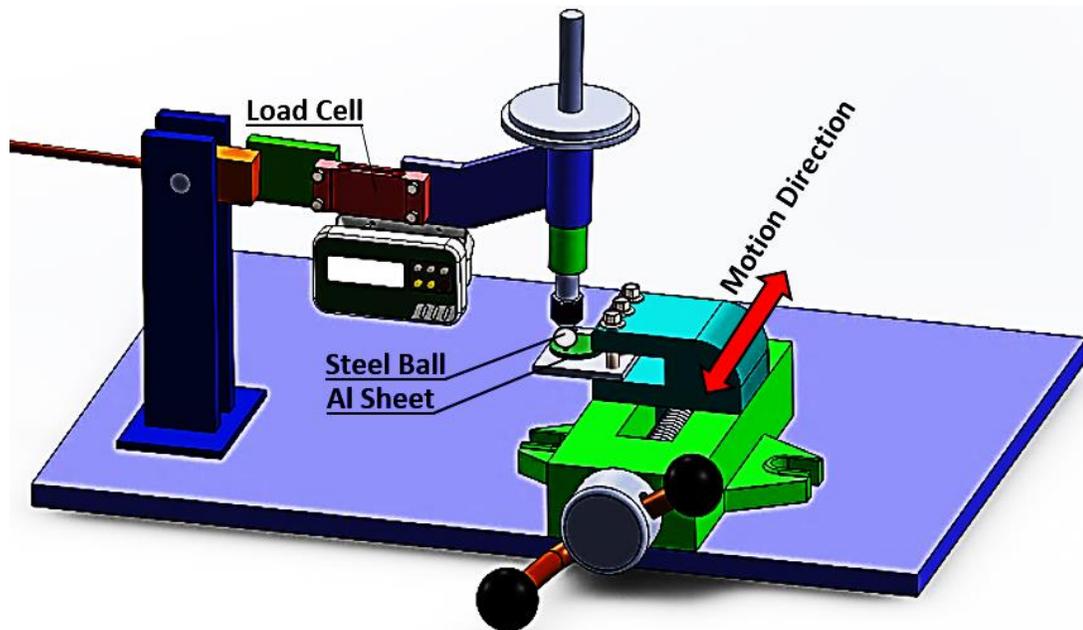


Fig. 1 Arrangement of the test rig.

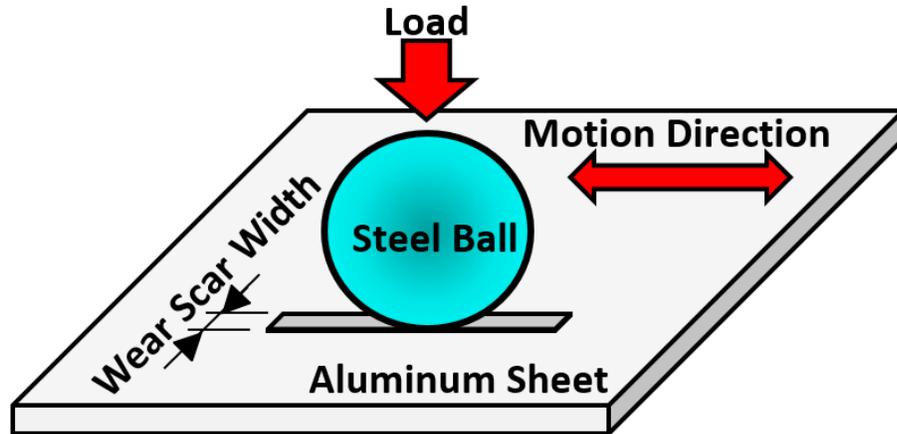


Fig. 2 Details of the test process.

The dispersing additives used were  $\text{Al}_2\text{O}_3$  nanoparticles of 30 – 50  $\mu\text{m}$  particle size and CNT of 10-30  $\mu\text{m}$  length. The nanomaterials were added in different contents of 0.2, 0.4, 0.6, 0.8 and 1.0 wt. %.

### RESULTS AND DISCUSSION

Friction coefficient displayed by the grease dispersed by CNT displayed the highest values followed by  $\text{Al}_2\text{O}_3$ , while CNT/ $\text{Al}_2\text{O}_3$  dispersing the grease showed the lowest values, Fig. 3. Friction coefficient slightly decreased down to minimum then increased with increasing nanomaterial content. Minimum values were observed at 0.4 – 0.6 wt. % of nanomaterial content. Further increase in nanomaterial content increased friction coefficient up to values higher than that recorded for grease free of nanomaterial. That behavior was more pronounced for CNT. It seems that agglomeration of CNT increased their layers and consequently shear stress increased.

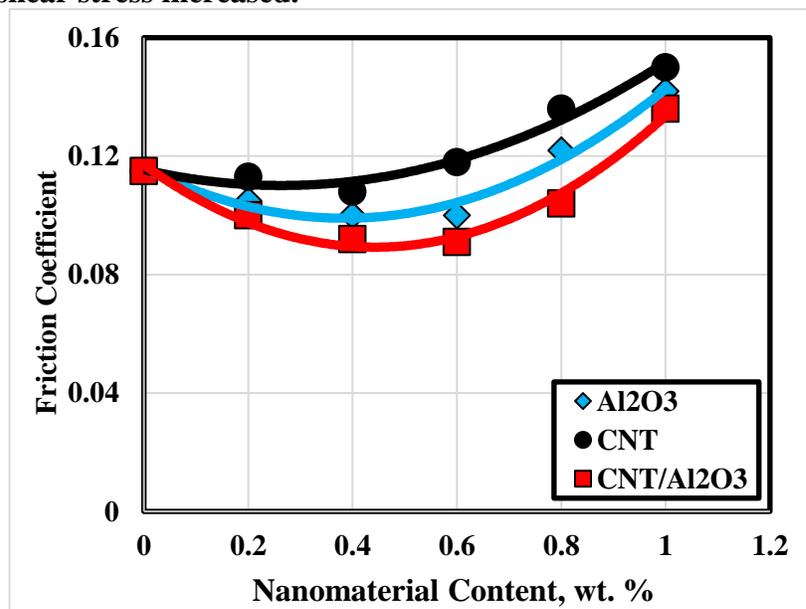


Fig. 3 Friction coefficient displayed by the tested nanomaterials dispersed in grease.

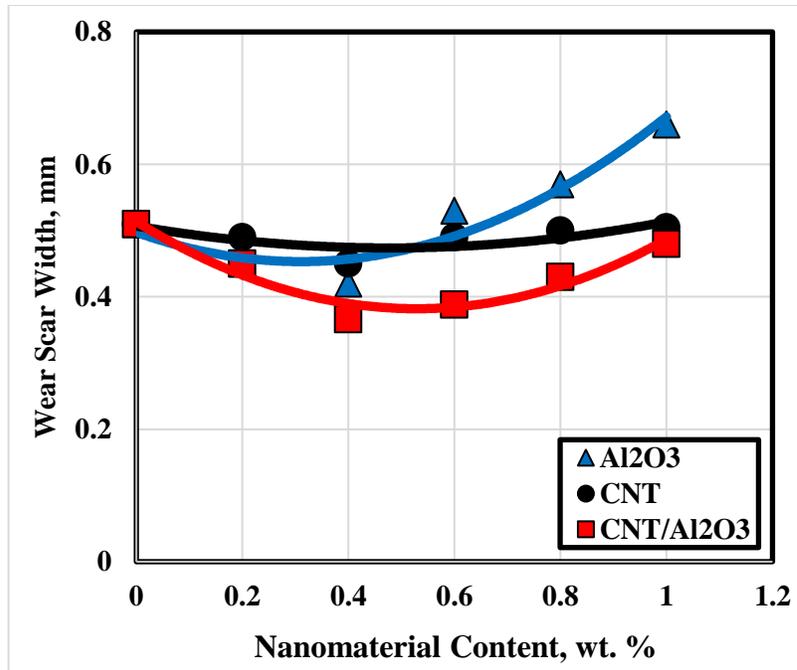


Fig. 4 Wear displayed by the tested nanomaterials dispersed in grease.

Al<sub>2</sub>O<sub>3</sub> showed relatively lower increase in friction due to the ball bearing effect of the nanoparticles. The enhancing effect of CNT/Al<sub>2</sub>O<sub>3</sub> may be attributed to the easy rolling of Al<sub>2</sub>O<sub>3</sub> nanoparticles by the help of the low shear CNT.

Wear of the test specimen measured by the wear scar width, Fig. 4, showed the same trend observed for friction. Minimum values were displayed by grease dispersed by CNT/Al<sub>2</sub>O<sub>3</sub> of 0.4 wt. % content. Further increase in Al<sub>2</sub>O<sub>3</sub> content significantly increased wear due to their abrasive action.

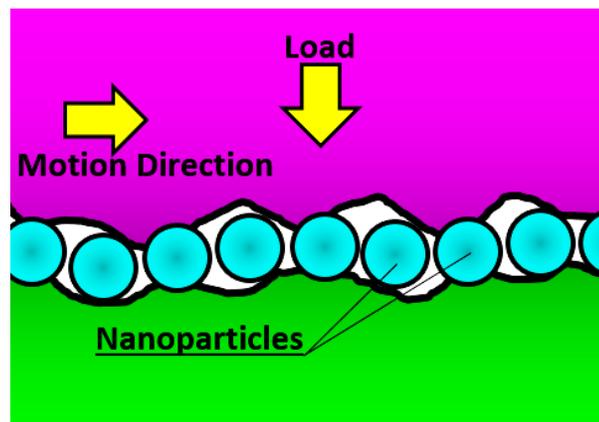


Fig. 1 Effect of ball bearing mechanism.

The mechanism of ball bearing depends on the size of the particles that should be bigger than the minimum film thickness to support the load, Fig. 1. Besides, the hardness of the

particles should be higher than the hardness of the two sliding surfaces. In the presence of nanoparticles, that mechanism can be valid for the very fine surfaces. In extreme pressure, nanoparticles can perform better due to their interaction with the asperities of surface roughness. Further increase of  $\text{Al}_2\text{O}_3$  nanoparticles increased wear as result of the increased abrasiveness. They act as rolling bearings separating the two contact surfaces, where metal to metal contact is prevented. The drawback is their fracture when the load is increased and the rolling action is retarded, [16 – 20].

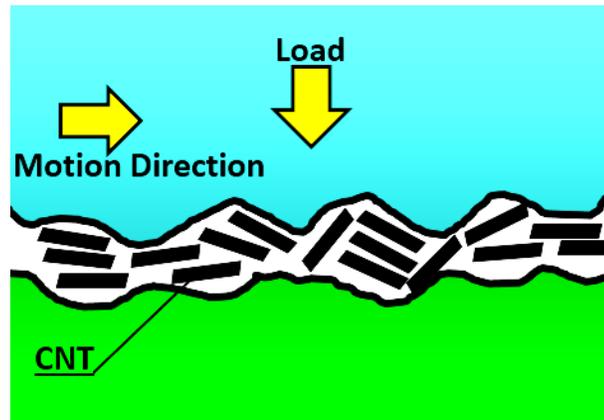


Fig. 2 Carbon nanotubes dispersed in grease.

The enhancement of the wear resistance offered by CNT might be attributed to the fact that CNT is quite good solid lubricant. The lubrication mechanism of CNT depends on their nature as cylinders. Their nanosize enables them entering into and adsorbing on the asperities of the rubbing surfaces, Fig. 2. It was found that their carbon content displayed significant reduction in friction due to the carbon formation on the friction surface of low shear strength film that protected from further friction and wear.

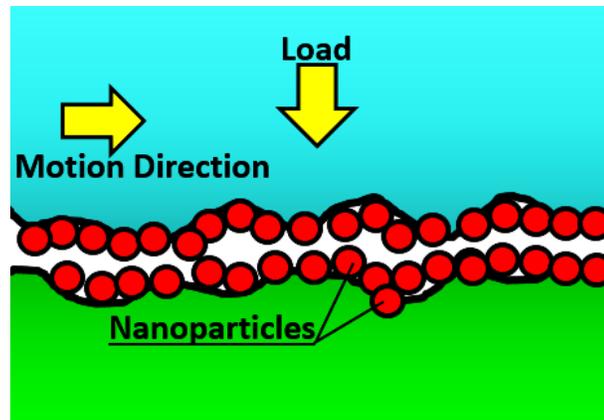


Fig. 3. Adhesion of  $\text{Al}_2\text{O}_3$  into the sliding surfaces.

CNT can be adsorbed onto the sliding surfaces forming physical adsorption film, Fig. 6. They can provide the surface by chemical reaction film and enhance the wear resistance [21 - 23]. The nanomaterials forms thin layer of high plasticity on the sliding surface. The extremely plastic film works as a viscous lubricant. It was revealed that, presence of the

transmitted film when formed from a material softer than the substrate, prevents seizure and tearing in depth.

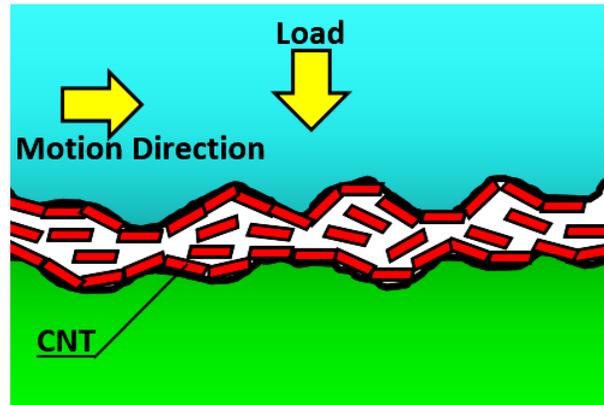


Fig. 4 Adhesion of CNT into the sliding surfaces.

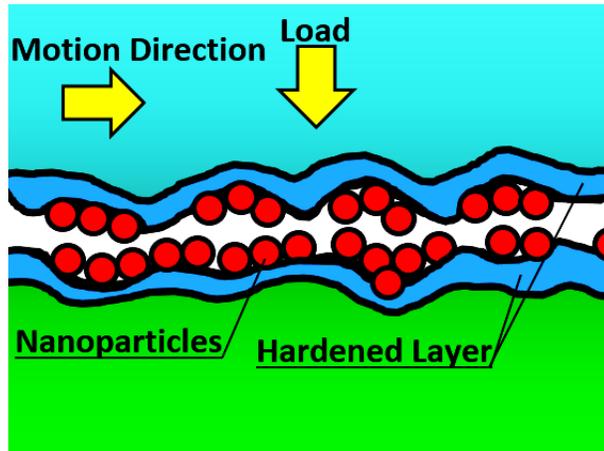


Fig. 5 Formation of hardened layers.

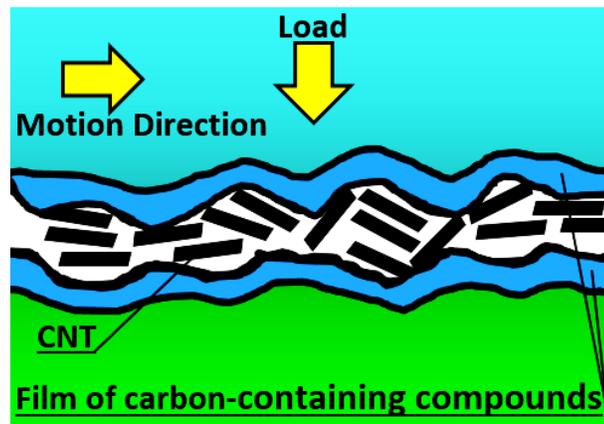


Fig. 6 Formation of carbon-containing compounds.

The presence of hard nanoparticles between the sliding surfaces prevented their direct contact, [26 - 28]. CNT deformed under the load, while Al<sub>2</sub>O<sub>3</sub> caused severe plastic deformation on test specimen and the scratch depth increased, Fig. 7. Al<sub>2</sub>O<sub>3</sub> nanoparticles acted as ball bearings sliding and rolling on the sliding surfaces accompanied by polishing effect. The ball bearing effect decreased the formation of the transfer layer, [27 - 30]. It was revealed that the friction of Al<sub>2</sub>O<sub>3</sub> nanoparticles reduce wear rate and enhance the morphology of the worn surface. The ball bearing mechanism offers wear and friction reduction by hard nanoparticles, where Al<sub>2</sub>O<sub>3</sub> nanoparticles roll between the rubbing surfaces. In addition to that, Al<sub>2</sub>O<sub>3</sub> nanoparticles polish the asperities and penetrate the contact area improving the morphology of the rough surface.

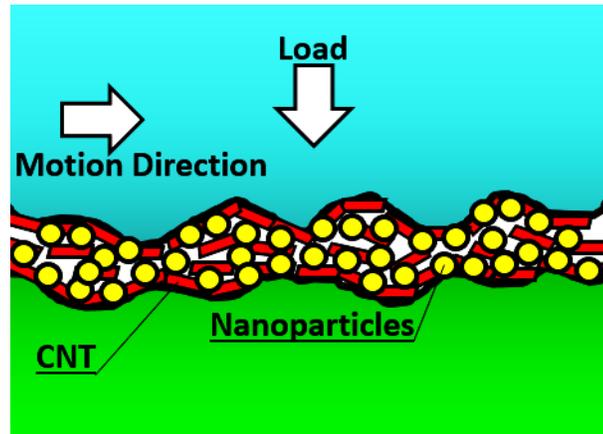


Fig. 7 CNT and Al<sub>2</sub>O<sub>3</sub> dispersed in grease.

In the present experiments, the friction coefficient and wear of CNT/Al<sub>2</sub>O<sub>3</sub> nanoparticles were studied. It is expected that the surface is adhered by film of carbon-containing compounds. It seems that CNT/Al<sub>2</sub>O<sub>3</sub> are transferred onto the surface. Based on that, nanoparticles change sliding friction into a combination of sliding friction as result of CNT and rolling friction because of Al<sub>2</sub>O<sub>3</sub> nanoparticles.

The mechanism of action of CNT/Al<sub>2</sub>O<sub>3</sub> depend on the fact that they enter the friction surfaces and form the third body that bear the shear force acting on the surface asperities. CNT dispersed in lithium is absorbed onto the sliding surface. They form protective film and prevent the direct contact between the asperities of the two surfaces. Besides, their relatively low shear strength causes interlayer sliding of relatively low friction. It is known that agglomeration of nanoparticles increases friction due to the reduced shear and ball bearing effects.

The shape of nanomaterial influences its performance in lubrication process. This can be explained on the bases of the nature of the contact between the nanoparticles and the contact area. Spherical nanoparticles have high load carrying capacity and EP properties due to their ball bearing effect, [31]. They have point contact with the sliding surfaces, while the line contact is resulted from interaction of CNT with the sliding surfaces. The morphology of nanoparticles is much affected by their internal nanostructure, [32]. The structure of CNT has a tendency to form tribo-films on the sliding surfaces and can withstand severe working conditions. It can be concluded that combination of CNT/Al<sub>2</sub>O<sub>3</sub>

results in significant improvement in the reduction of friction and wear. It seems that the agglomeration of nanoparticles decreased allowing the nanomaterial to behave in efficient way.

## CONCLUSIONS

1. Friction coefficient displayed by the grease dispersed by CNT displayed the highest values followed by  $\text{Al}_2\text{O}_3$ , while CNT/ $\text{Al}_2\text{O}_3$  dispersing the grease showed the lowest values.
2. Friction coefficient slightly decreased down to minimum then increased with increasing nanomaterial content. Minimum values were observed at 0.4 – 0.6 wt. % of nanomaterial content.
3. Minimum wear values were displayed by grease dispersed by CNT/ $\text{Al}_2\text{O}_3$  of 0.4 wt. % content. Further increase in  $\text{Al}_2\text{O}_3$  content significantly increased wear due to their abrasive action.
4. The lubrication mechanism of CNT depends on the carbon formation of low shear strength film on the friction surface that protected from further friction and wear, while  $\text{Al}_2\text{O}_3$  nanoparticles act as ball bearing and offer wear and friction reduction, where  $\text{Al}_2\text{O}_3$  nanoparticles roll between the rubbing surfaces. Besides,  $\text{Al}_2\text{O}_3$  nanoparticles polish the asperities and penetrate the contact area improving the morphology of the rough surface.
5. Further increase of  $\text{Al}_2\text{O}_3$  nanoparticles increased wear as result of the increased abrasion.
6. Combination of CNT/ $\text{Al}_2\text{O}_3$  significantly reduced friction and wear.

## REFERENCES

1. Hasouna A. T., Samy A. M., Ali W. Y., "Influence of Solid Lubricants on Reducing Friction and Wear Caused by Sand Contaminating Greases", MEATIP5 Conference, Assiut University, Assiut, Egypt, 29 – 31 March 2011, (2011).
2. Khashaba M. I., Youssef M. M., Ali W. Y., "Mechanism of Action of Lubricating Greases Dispersed by Polymeric Powders, Graphite and Molybdenum Disulphide", MEATIP5 Conference, Assiut University, Assiut, Egypt, 29 – 31 March 2011, (2011).
3. Mota V., and Ferreira L. A., "Influence of Grease Composition on Rolling Contact Wear: Experimental Study", Tribology International 42, pp. 569 – 574, (2009).
4. Cann P. M., "Grease Lubrication of Rolling Element Bearings - Role of Grease Thickener", Lubr. Sci. 19, pp. 183 – 196, (2007).
5. Couronne I., Vergne P., Mazuyer D., Truong-Dinh N., Girodin D., "Effects of Grease Composition and Structure on Film Thickness in Rolling Contact", Tribol. Trans., 46 (1), pp. 31 – 26, (2003).
6. Kim H. and Kardes N., "Friction and Lubrication", Sheet Met. Forming Fundamentals, ASM International, (2012).
7. Kirkhorn L., Bushlya V., Andersson M., and Stahl J. E., "The Influence of Tool Steel Microstructure on Friction in Sheet Metal Forming", Wear, Vol. 302, No. 1 - 2, pp. 1268 - 1278, Apr. (2013).
8. Choi I. S., Joun M. S., Moon H. G., Lee M. C. and Jun B. Y., "Effects of Friction Laws on Metal Forming Processes", Tribology International, Vol. 42, pp. 311–319, (2009).
9. Bay N., Olsson D. D. and Andreasen J. L., "Lubricant Test Methods for Sheet Metal Forming", Tribol. Int., Vol. 41, No. 9 - 10, pp. 844 - 853, Sep. (2008).

10. Rajesh E. and Prakash M. S., “Analysis of Friction Factor by Employing the Ring Compression Test Under Different Lubricants”, *International Journal of Scientific & Engineering Research*, Volume 4, Issue 5, pp. 1163 – 1171, (2013).
11. Hasan S., Rasty J., “Determination of Friction Coefficient Utilizing the Ring Compression Test”, *Journal of Engineering Materials and Technology*, pp. 338 - 348, (2001).
12. Jeswiet J., Arentoft M., and Henningsen P., “Methods and Devices Used to Measure Friction in Rolling”, *IMEchE Proc. IMechE Vol. 220 Part B: J. Engineering Manufacture*, pp. 49 – 57, (2006).
13. Fereshteh-Saniee F., Pillinger I., Hartley P., “Friction Modelling for the Physical Simulation of the Bulk Metal Forming Processes”, *Journal of Material Processing Technology*, pp. 153 - 154, pp. 151-156, (2004).
14. Peng D. X., Kang Y., Hwang R. M., Shyr S. S., Chang Y. P., “Tribological Properties of Diamond and SiO<sub>2</sub> Nanoparticles Added in Paraffin”, *Tribology international*, 42, pp. 911 - 917, (2009).
15. EL-Abden S. Z., “Effect of Silica Nanoparticles and Multiwall Carbon Nanotubes Dispersing Lubricating Grease in Metal Forming”, *Egtrib*, Vol. 16, No. 4, October 2019, pp. 15 – 24, (2019).
16. Choi Y., Lee C., Hwang Y., Park M., Lee J., Choi C., et al., “Tribological Behavior of Copper Nanoparticles as Additives in Oil”, *Curr. Appl. Phys.*, 9, pp. 124 - 127, (2009).
17. Peng D. X., “Tribological Properties of Diamond and SiO<sub>2</sub> Nanoparticle Added in Paraffin”, (42), *Tribology International*, pp. 911 - 917, (2009).
18. Peng D. X., “Size Effect of SiO<sub>2</sub> Nanoparticle as Oil Additives on Tribology of Lubricant”, *Industrial Lubrication and Tribology*, (62), pp. 111- 120, (2018).
19. Jio D., “The Tribology Properties of Alumina/Silica Composite Nanoparticle as Lubricant Additives”, *Appl. Surf. Sci.*, 257 (13), pp. 5720 - 5725, (2011).
20. Lopez T. D., “Engineered Silica Nanoparticle as Additives in Lubricant Oils”, (16), *Sci. Technol. Adv. Material*, (16), pp. 23 – 34, (2015).
21. Liu L., Ming Z., Jin L., Li L., Mo Y., Su G., Li X., Hu H. Z., Tian Y., “Recent Advances in Friction and Lubrication of Graphene and other 2D Materials”, *Mechanisms and applications*, *Friction* 7, (3), pp. 199 - 216 (2019).
22. Xiao H. P., Liu S. H., “2D Nanomaterials as Lubricant Additive”, *A Review. Mater. Des.* 135, pp. 319 - 332 (2017).
23. Tao X., Jiazheng Z., Kang. X., “The Ball-Bearing Effect of Diamond Nanoparticles as an Oil Additive”, *J. Phys. D., Appl. Phys.*, 29, pp. 2932 - 2937, (1996).
24. Peng D. X., Kang Y., Chen C. H ,Chen S. K , Shu F., “The Tribological Behavior of Modified Diamond Nanoparticles in Liquid”, *Ind. Lubr. Tribol.*, 61, pp. pp. 213 - 219, (2009).
25. Peng D. X., Chen C. H., Kang Y., Chang Y. P., Chang S. Y., “Size Effects of SiO<sub>2</sub> Nanoparticles as Oil Additives on Tribology of Lubricant”, *Ind. Lubr. Tribol.*, 62, 111 – 120, (2010).
26. Hu C., Bai M., Lv J., Kou Z., Li X., “Molecular Dynamics Simulation on the Tribology Properties of Two Hard Nanoparticles (Diamond and Silicon Dioxide) confined by two Iron Blocks”, *Tribology International*, 90, pp. 297 – 305, (2015).

27. Hu C., Bai M., Lv J., Liu H., Li X., “Molecular Dynamics Investigation of the Effect of Copper Nanoparticle on the Solid Contact Between Friction Surfaces”, *Appl. Surf. Sci.*, 321, pp. 302 - 309, (2014).
28. Chou C. C., Lee S. H., “Rheological Behavior and Tribological Performance of a Nanodiamond-Dispersed Lubricant”, *J Mater Process Technol*, 201, pp. 542 - 547, (2008).
29. Sia S. Y., Sarhan A. A. D., “Morphology Investigation of Worn Bearing Surfaces using SiO<sub>2</sub> Nanolubrication System”, *Int. J. Adv. Manuf. Technol.*, 70, pp. 1063 - 1071, (2014).
30. Luo T., Wei X., Huang X., Huang L., Yang F., “Tribological Properties of Al<sub>2</sub>O<sub>3</sub> Nanoparticles as Lubricating Oil Additives”, *Ceram. Int.* 40, pp. 7143 - 7149, (2014).
31. Rabaso P., “Boundary Lubrication: Influence of the Size and Structure of Inorganic Fullerene-Like MoS<sub>2</sub> Nanoparticles on Friction and Wear Reduction”, *Wear*, 320, pp. 161 - 178, (2014).