



## **FRICITION COEFFICIENT DISPLAYED BY SLIDING RUBBER ON EPOXY REINFORCED BY NATURAL FIBERS**

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### **ABSTRACT**

The relatively low static friction coefficient displayed by sliding of soles on floor tiles is considered as the major reason in walking accidents indoors. The present work studies the effect of reinforcing epoxy by natural fibers such as wood, rice straw and palm fibers on friction coefficient to guarantee the availability be used as floor material and enhance the tribological and mechanical properties.

The experimental observations revealed that wood fibers reinforced composites displayed friction coefficient of values higher than that recommended in the universal building codes (0.5). It was found that friction coefficient slightly decreased with as the fiber content increased. While, significant increase in friction coefficient was caused as the applied load increased due to the increase of the contact area. Rice straw fibers experienced lower values of friction coefficient compared to wood fibers. Further decrease in friction coefficient was observed for composites reinforced by palm fibers.

### **KEYWORDS**

Friction coefficient, sliding, rubber, epoxy, natural fibers.

### **INTRODUCTION**

The probability of slip of foot walking on floor tiles increases and consequently accidents occur when the static friction coefficient is low. The slip and falling are related to the floor materials, contaminants, and surface properties of the sole. The slip resistance is quantified using the static coefficient of friction. The static friction coefficient of 0.5 has been recommended as standard for unloaded, normal walking conditions in USA, [1]. The static friction coefficient values should be increased for safe walking when handling loads. In Europe, [2 - 4], Friction coefficient ( $\mu$ ) should be 0.3 or more, while the floor with the friction coefficient between 0.15 and 0.05 was very slippery. Several building codes have established that  $\mu \geq 0.50$  is the minimum slip resistance for safe floor surfaces. While,  $\mu \geq 0.60$  for walkways and elevators as well as  $\mu \geq 0.80$  for ramps, [5]. The effect of the thickness on the frictional behaviour

of polymers filled by recycled polyurethane tiles was investigated, [6, 7]. Rubber mats compared to ceramic and polymeric tiles showed the highest friction values.

It was found that filling floor tiles by rubber leads to a higher contact area and more pronounced deformations when mechanically interacting and sliding on rigid material. Higher friction coefficients can be expected for rubber than for relatively harder polymers, [8, 9]. The friction coefficient difference between dry and wet surfaces depended on the footwear material and floor combinations, [10 - 14]. Friction measurements under liquid-contaminated depend on the squeeze film theory that explains the influence of the liquid on the friction values.

The tribological and mechanical properties of epoxy were enhanced by filling by rubber, [15 – 17], where rubber particles could increase the ductility and plastic deformation of epoxy. Fracture toughness could be significantly developed by adding copolymer, [18], by reducing the cracks and shear yielding of the matrix, [19 - 21]. Presence of rubber inside epoxy matrix increases the shear deformation and improves fracture toughness and consequently reduce the brittleness of epoxy resins.

Filling epoxy by recycled polymers was investigated, [22, 23]. Toughening of epoxy by filling with recycled rubber granulates was investigated, [24 - 29], to make full use of the deformation and higher contact area during loading on the rigid surfaces. Therefore, high values of friction coefficient and abrasion resistance of epoxy floor tile can be enhanced by rubber, [30 - 32]. Tribological properties of epoxy was improved by adding oil during molding, where significant reduction in friction was observed, [33 – 37]. This behavior was attributed to the oil trapped in pores after solidification that fed into the sliding surface.

In the present work, epoxy was reinforced by natural fibers such as wood, rice straw and palm fibers in contents up to 20 wt. % and tested through sliding on rubber to determine friction coefficient at dry sliding condition.

## **EXPERIMENTAL**

Experiments were carried out to determine the friction coefficient displayed by the sliding of the tested epoxy composites on rubber surface. The test rig is shown in Fig. 1. The epoxy composites of 5.0 mm thickness were molded to one surface of wooden cube of  $30 \times 30 \times 30 \text{ mm}^3$ . After solidification, they were loaded into rubber sheet of 8.0 mm thickness of 60 Shore D hardness. The rubber sheet was adhered into the base of the test rig that was supported by two load cells, the first measured the friction force and the second measured the applied load.

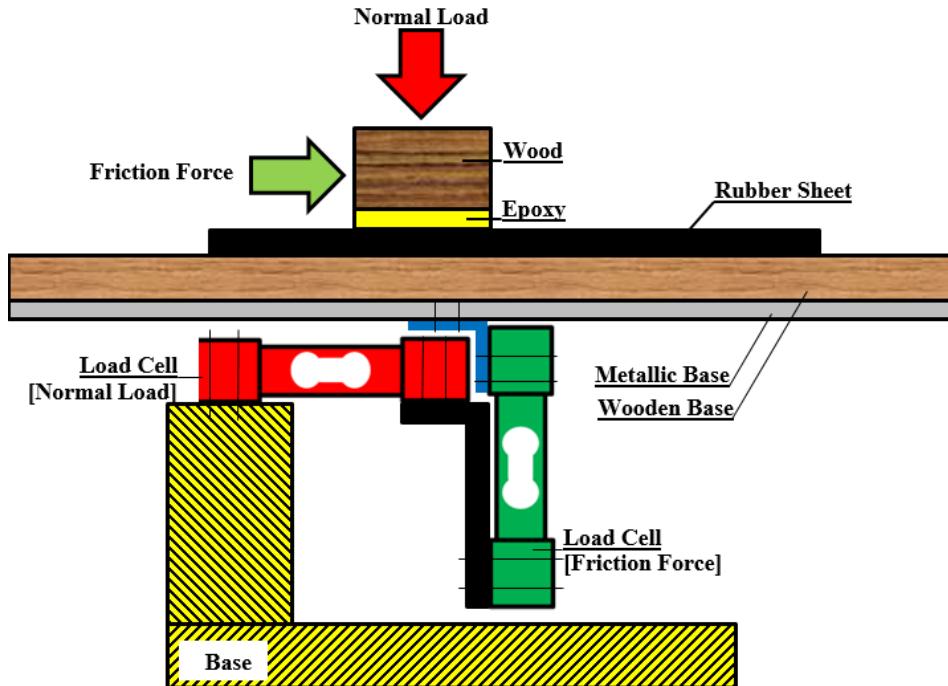


Fig. 1 Arrangement of the adhesive test rig.

Epoxy was reinforced by wood, rice straw and palm fibers of (0 - 1.0 mm), (0 - 1.0 mm) and (0 - 3.0 mm) granulate size respectively. The natural fibers were added in contents of 2.5, 5.0, 7.5, 10, 12.5, 15, 17.5 and 20 wt. %, where every experiment was repeated five times then the average values were considered. The tests were carried out at different values of normal load (2, 4, 6 and 8 N) applied by weights.

## RESULTS AND DISCUSSION

It is well known that the lowest permissible value of the static friction coefficient is 0.5 recommended for floor surfaces. For disables, walkways and elevators, this value should be increased to 0.6 – 0.8. It is necessary to apply materials of high contact area and deformation to obtain high values of friction coefficient. The results of friction coefficient displayed by the tested composites are shown in Figs. 2 - 4. The values of friction coefficient observed for composites reinforced by wood fibers were higher than the recommended values mentioned above. Generally, friction coefficient decreased with increasing the wood content. As the applied load increased friction coefficient increased due to the increase of the contact area.

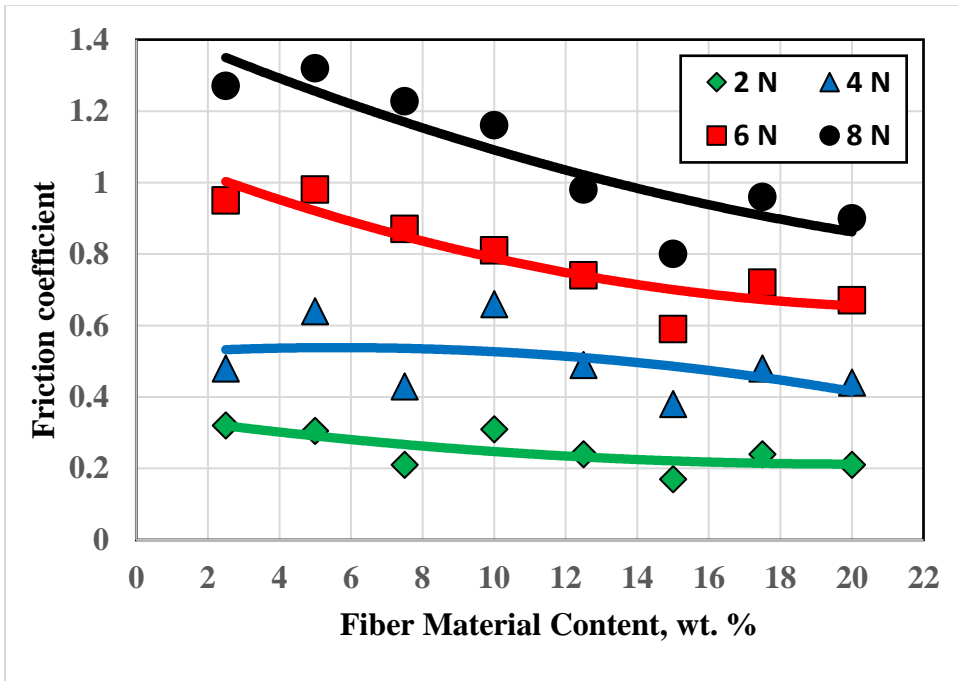


Fig. 2 Friction coefficient displayed by sliding of the tested composites reinforced by wood fibers.

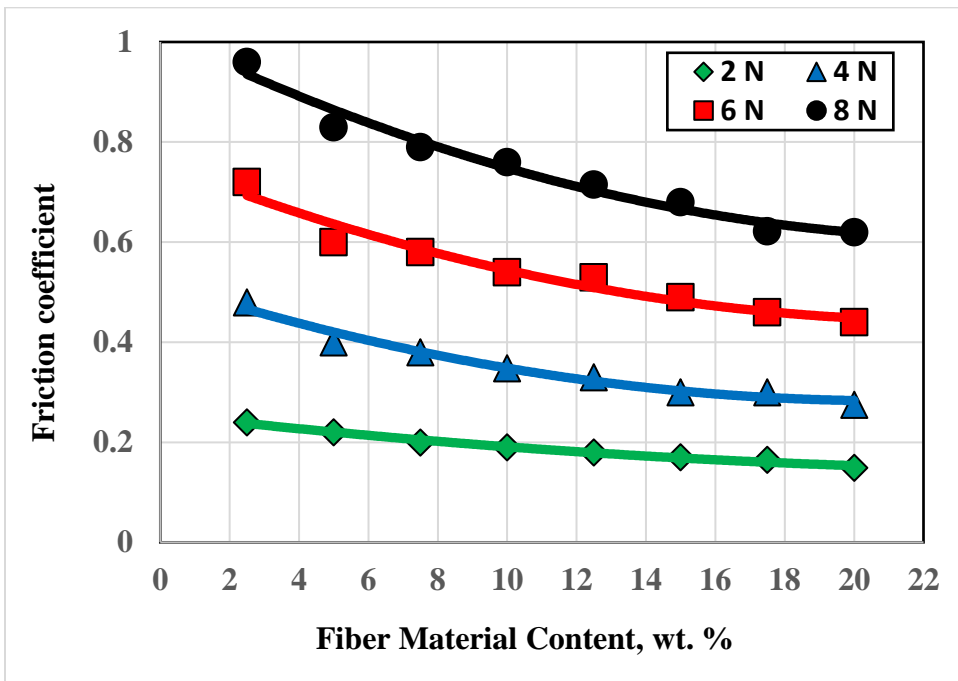
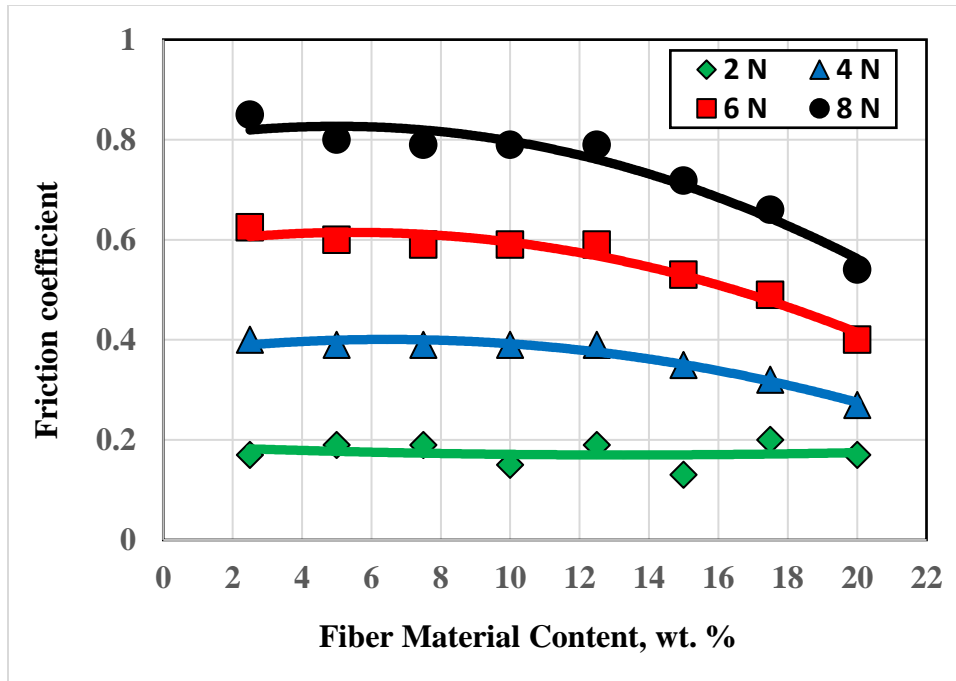


Fig. 3 Friction coefficient displayed by sliding of the tested composites reinforced by rice straw fibers.



**Fig. 4** Friction coefficient displayed by sliding of the tested composites reinforced by palm fibers.

Reinforcing epoxy by rice straw fibers displayed lower values of friction coefficient, Fig. 3, compared to that observed for composites reinforced by wood fibers. The highest friction coefficient values were displayed by composites containing lower fiber content. At 8.0 N load, the friction values were 0.96 and 0.62 at 2.5 and 20 wt. % fiber content respectively. Further friction decrease was observed during sliding of the tested composites reinforced by palm fibers, Fig. 4, where friction coefficient values recorded at 8.0 N load, were 0.85 and 0.54 at 2.5 and 20 wt. % fiber content respectively.

## CONCLUSIONS

1. Values of friction coefficient displayed by composites reinforced by wood fibers were higher than the recommended values mentioned in the universal building codes (0.5).
2. The objective of filling epoxy by natural fibers is to enhance the tribological and mechanical properties. That was achieved by the tested natural fibers.
3. Friction coefficient slightly decreased with increasing the fiber content.
4. Increasing the applied load caused significant increase in friction coefficient due to the increase of the contact area.
4. Rice straw fibers reinforcing epoxy showed lower values of friction coefficient than observed for wood fibers.
5. Composites reinforced by palm fibers showed further decrease in friction coefficient compared to wood and rice straw fibers.

## REFERENCES

1. Miller J. M., "“Slippery” work surface: toward a performance definition and quantitative coefficient of friction criteria", *J. Saf. Res.* 14, pp. 145 - 158, (1983).
2. Grönqvist R., "Mechanisms of friction and assessment of slip resistance of new and used footwear soles on contaminated floors", *Ergonomics* 38, pp. 224 - 241, (1995).
3. Myung, R., Smith, J. L., Leamon, T. B., "Subjective assessment of floor slipperiness", *Int. J. Ind. Ergon.* 11, pp. 313 - 319, (1993).
4. Kai W. L., Rui-feng Y., Xiao L. H., "Physiological and psychophysical responses in handling maximum acceptable weights under different footwear–floor friction conditions", *Applied Ergonomics* 38, pp. 259 – 265, (2007).
5. Burnfield J. M., Tsai Y. J., Powers Ch. M., "Comparison of utilized coefficient of friction during different walking tasks in persons with and without a disability", *Gait & Posture* 22, pp. 82 – 88, (2005).
6. Elham B. R., Khashaba M. I. and Ali W. Y., "Friction coefficient of recycled rubber floorings: I. effect of rubber tile thickness, to be published.
7. El-Sherbiny Y. M., Mohamed M. K. and Ali W. Y., "Prevention of Slip Accidents by Using Rubber Floor Mat", *Journal of the Egyptian Society of Tribology* Vol. 9, No. 1, January 2012, pp. 24 – 38, (2012).
8. Derler S., Kausch F., Huber R., "Analysis of factors influencing the friction coefficients of shoe sole materials", *Safety Science* 46, pp. 822 - 832, (2008).
9. Maeda K., Bismarck A., Briscoe B., "Effect of bulk deformation on rubber adhesion ", *Wear* 263, pp. 1016 – 1022, (2007).
10. Samy A. M., Mahmoud M. M., Khashaba M. I. and Ali W. Y., "Friction of Rubber Sliding Against Ceramics, I. Dry And Water Lubricated Conditions", *KGK Kautschuk Gummi Kunststoffe* 60. Jahrgang, Nr 607, Juni 2007, pp. 322 – 327, (2007).
11. Samy A. M., Mahmoud M. M., Khashaba M. I. and Ali W. Y., "Friction of Rubber Sliding Against Ceramics, II. Oil And Oil Diluted By Water Lubricated Conditions", *KGK Kautschuk Gummi Kunststoffe* 60. Jahrgang, Nr 607, December 2007, pp. 693 – 696, (2007).
12. Samy A. M., Mahmoud M. M., Khashaba M. I. and Ali W. Y., "Friction of Rubber Sliding Against Ceramics, III. Sand Contaminating the Lubricating Fluids", *KGK Kautschuk Gummi Kunststoffe* 60. Jahrgang, Nr 607, January/February 2008, pp. 43 – 48, (2008).
13. Ezzat F. H., Hasouna A. T., Ali W. Y., "Friction Coefficient of Rubber Sliding Against Polymeric Indoor Flooring Materials of Different Surface Roughness", *Journal of the Egyptian Society of Tribology*, Vol. 4, No. 4, January 2007, pp. 37 – 45, (2007).
14. Chang W. R., "The effect of surface roughness on the measurements of slip resistance", *International Journal of Industrial Ergonomics* 24(3), pp 299 – 313, (1999).
15. Eman S. M, Khashaba M. I. and Ali W. Y., "Friction Displayed by the Sliding of Rubber on Epoxy Filled by Recycled Rubber Particle", *Journal of the Egyptian Society of Tribology*, Vol. 18, No. 3, July 2021, pp. 1 – 10, (2021).
16. Eman S. M, Khashaba M. I., Eyad M. A. and Ali W. Y., "Electrostatic Charge Generated from Sliding of Rubber on Epoxy Filled by Recycled Rubber Granulates",

**Journal of the Egyptian Society of Tribology, Vol. 18, No. 4, October 2021, pp. 45 – 54, (2021).**

**17. Eman S. M., Khashaba M. I. and Ali W. Y., “Friction and Wear Displayed by the Scratch of Epoxy filled by recycled Rubber Particles”, *KGK Kautschuk Gummi Kunststoffe*, 2022, 75(6), pp. 35–38, (2022).**

**18. Bagheri R., Marouf B. T., Pearson R. A. “Rubber-toughened epoxies: a critical review”, *Polym Rev* 49, pp. 201 - 225, (2009).**

**19. Liang Y. L., Pearson R. A., “The toughening mechanism in hybrid epoxy-silica-rubber nanocomposites”, *Polymer* 51, pp. 4880 - 4890, (2010).**

**20. Chen J., Kinloch A. J., Sprenger S., Taylor A. C., “The mechanical properties and toughening mechanisms of an epoxy polymer modified with polysiloxane-based core-shell particles”, *Polymer* 54, pp. 4276 - 4289, (2013).**

**21. Lorena R. P., Royston G. J., Fairclough P. A., Ryan A. J., “Toughening by nanostructures”, *Polymer* 49, pp. 4475 - 4488, (2008).**

**22. Liu J., Thompson Z. J., Sue H. J., Bates F. S., Hillmyer M. A., Dettloff M. V., Jacob G., Verghese N., Pham H., “Toughening of epoxies with block copolymer micelles of wormlike morphology”, *Macromolecules* 43, pp. 7238 - 7243, (2010).**

**23. Declet-Perez C., Francis L. F., Bates F. S., “Deformation process in block copolymer toughened epoxies”, *Macromolecules* 48, pp. 3672 - 3684, (2015).**

**24. Marouf B. T., Mai Y. W., Bagheri R., Pearson R. A., “Toughening of epoxy nanocomposites: nano and hybrid effects. *Polym Rev* 54, pp. 56 – 78, (2016).**

**25. Khashaba M. I., Ezzat F. H. and Ali W. Y., “Mechanical and Tribological Properties of Recycled Polymers”, *Proceedings of The International Conference of Development and Environment, Assiut University, March 26 – 28, Assiut, Egypt*, pp. 381 – 390, (2002).**

**26. Khashaba M. I. and Ali W. Y., “Mechanical Properties of Epoxy Filled by Recycled Polymeric Powders”, *Proceedings of The International Conference of Development and Environment, Assiut University, March 26 – 28, Assiut, Egypt*, pp. 373 – 379, (2002).**

**27. Ho R. M., Wu C. H., Su A. C., “Morphology of plastic/rubber blends”, *Polym. Eng. Sci.* 30 (9), pp. 511 - 518, (1990).**

**28. Jang, B. Z., Uhlmann, D. R., Vander Sande, J.B., “Crystalline morphology of polypropylene and rubber-modified polypropylene”, *J. Appl. Polym. Sci.* 29 (12), pp. 4377 – 4393, (1984).**

**29. Montoya M., Tomba J. P., Carella J. M., Gobernado-Mitre, M.I., “Physical characterization of commercial polyolefinic thermoplastic elastomers”, *Eur. Polym. J.* 40 (12), pp. 2757 - 2766, (2004).**

**30. Lia K. W., Chang C. C., Chang W. R., “Slipping of the foot on the floor when pulling a pallet truck”, *Applied Ergonomics* 39, pp. 812 - 819, (2008).**

**31. Derler S., Kausch F., Huber R., “Analysis of factors influencing the friction coefficients of shoe sole materials”, *Safety Science* 46, pp. 822 - 832, (2008).**

**32. Maeda K., Bismarck A., Briscoe B., “Effect of bulk deformation on rubber adhesion”, *Wear* 263, pp. 1016 – 1022, (2007).**

**33. Badran A. H., Hasan M. K., Ali W. Y., "Tribological Behavior of Epoxy Reinforced with Carbon Nanotubes and Filled by Vegetables Oils", *EGTRIB Journal*, Vol. 14, No. 1, January 2017, pp. 51 - 61, (2017).**

34. Eatemad H. S., Samy A. M. Khashaba M. I., and Ali Y. A., "Friction and Wear of Polymeric Materials Filled by Oil and Reinforced by Nanocarbon Tubes", *EGTRIB Journal*, Vol. 14, No. 4, October 2017, pp. 15 – 26, (2017).
35. Hassan A. El-Sayed M., Eid A. I., El-Sheikh M., Ali W. Y., "Tribological Properties of Low Density Polyethylene and Polyamide 12 as Polymer Matrix Nanocomposites", *EGTRIB Journal*, Vol. 14, No. 4, October 2017, pp. 40 – 53, (2017).
36. Hassan A. El-Sayed M., Eid A. I., El-Sheikh M., Ali W. Y., "Effect of Graphene Nanoplatelets and Paraffin Oil Addition on the Mechanical and Tribological Properties of Low Density Polyethylene Nanocomposites", *Arabian Journal for Science and Engineering*, DOI 10.1007/s13369-017-2965-5, Published online: 15 November 2017, (2017).
37. Hassan A. E. M., Eid A. I., El-Sheikh M., Ali W.Y., "Mechanical and tribological performance of polyamide 12 reinforced with graphene nanoplatelets and paraffin oil nanocomposites", *Materialwiss. Werkstofftech.* 2019, 50, pp. 74 – 85, (2019).